Inclusive breakup calculations in angular momentum basis: Application to ⁷Li + ⁵⁸Ni

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The angular momentum basis method is introduced to solve the inclusive breakup problem within the model proposed by Ichimura, Austern, and Vincent [Phys. Rev. C 32, 431 (1985)]. This method is based on the geometric transformation between different Jacobi coordinates, in which the particle spins can be included in a natural and efficient way. To test the validity of this partial wave expansion method, a benchmark calculation is done comparing with the one given by Lei and Moro [Phys. Rev. C 92, 044616 (2015)]. In addition, using the distorted-wave Born approximation version of the IAV model, applications to $^7\text{Li} + ^{58}\text{Ni}$ reactions at energies around Coulomb barrier are presented and compared with available data.

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I. INTRODUCTION

Investigation of reaction mechanisms responsible for the large inclusive α particle production cross section observed in breakup of light-weakly bound projectiles (e.g., ^{6.8}He, ^{6.7}Li, and ^{7.9}Be) is a topic of current interest, both experimentally and theoretically [1–5]. This is a difficult problem, because different reaction mechanisms, like elastic breakup, transfer, compound nuclear evaporation, inelastic breakup, and incomplete fusion contribute to the α yield.

From the theoretical point of view, one can represent this kind of reactions as $a + A \rightarrow b + B^*$, where a = b + x and B^* is any possible state of x + A system. This reaction includes the breakup processes in which x is elastically scatted by A leaving all the fragments in the ground states, which is usually called elastic breakup (EBU), but also breakup accompanied by target excitation, particle(s) exchange between x and A, x transfer to A, the fusion of x by x, which are globally referred to as nonelastic breakup (NEB). The total breakup (TBU) is therefore the sum of EBU and NEB components.

The IAV model [6], which was originally proposed in the 1980s, is used to study this inclusive breakup. Due to the computational limitations at that time, this model was no longer used. Recently, the model has been re-examined by several groups [7–12]. Moreover, a systematic study of the α productions in ⁶Li induced reactions has been recently reported by Lei and Moro [13], in which the numerical calculations using the IAV model agree well with the experimental data.

For ${}^{7}\text{Li}$, several experimental groups have reported large α yields and tried to understand the origins of these α s by using Q-value considerations and by direct identification of the reaction products [2,14–16]. However, a proper interpretation of these α s is still lacking. The IAV model, which successfully reproduces the α s produced by ${}^{6}\text{Li}$ is a promising tool for this purpose. From the theoretical point of view, an important

difference between these two systems is that the $\alpha+d$ cluster in ^6Li is in a predominantly $\ell=0$ configuration, whereas the $\alpha+t$ cluster conforming the ^7Li system is in a $\ell=1$ configuration by assuming a two body structure of the projectile. This makes the numerical calculation more challenging since more angular momentum configurations are involved in the calculation.

For this reason, most applications of the IAV formalism have been restricted to deuterons and ^6Li . In order to extend the model to other interesting systems, it is advisable to test its validity and accuracy for $\ell>0$ cases. For that purpose, the problem of $^7\text{Li}+^{58}\text{Ni}$ at energies around Coulomb barrier is studied within the IAV model. The calculated results are also compared with experimental data [17].

In the paper, a new numerical method to compute the IAV inclusive breakup formula is implemented in a more efficient way. The derived formula has been tested for the $\ell=0$ case against the previously implemented method. This former method becomes numerically difficult for $\ell>0$ cases, due to the additional angular momentum couplings (details see Appendix B of Ref. [7]). Moreover, the inclusion of the intrinsic spins will make the calculation even harder. Consequently, an alternative method which can deal with these more complicated situations would be advisable.

The paper is organized as follows. In Sec. II the main formulas of the IAV model and the expansion in angular momentum basis are outlined. In Sec. III, the formalism is applied to inclusive breakup reactions induced by ⁷Li. Finally, in Sec. IV the main results are summarized.

II. THEORETICAL MODELS

In this section, I briefly summarize the model of IAV and introduce a more efficient method for partial wave expansion comparing with the one used in Ref. [7]. The new method is more general and easy to incorporate particle spins.

First, one can write the process under study in the form

$$a(=b+x) + A \to b + B^*, \tag{1}$$

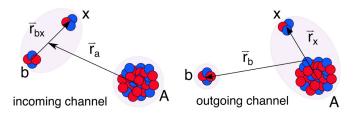


FIG. 1. Coordinates used in the breakup reaction.

where the projectile a, constituted by b and x, interacts with the target A, leaving particle b and other fragments. Thus B^* is any possible state between x + A system.

The effective three-body Hamiltonian of this system is

$$H(\xi) = H_0 + V_{bx} + V_{xA}(\xi) + U_{bA} + H_A(\xi), \qquad (2)$$

where H_0 is the total kinetic energy operator, V_{bx} is the interaction between the cluster b and x, $H_A(\xi)$ is the Hamiltonian of the target nucleus (with ξ denoting its internal coordinates), and V_{xA} and U_{bA} are fragment-target interactions.

In writing the Hamiltonian of the system in the form (2) I make a clear distinction between the two cluster constituents; the interaction with the target of the fragment b, the one which is assumed to be observed in the experiment, is described with a (complex) optical potential. Nonelastic processes arising from this interaction (e.g., target excitation, transfer, sequential breakup, and incomplete fusion) are included only effectively through the imaginary part of U_{bA} . Then particle b is said to act as a spectator. On the other hand, the interaction of the particle x with the target retains the target degrees of freedom (ξ).

By using the closure relation and optical reduction, IAV separated the inclusive breakup cross section in terms of elastic breakup and nonelastic breakup, with the latter is given by

$$\frac{d^2\sigma}{dE_b d\Omega_b}\bigg|_{\text{NEB}} = -\frac{2}{\hbar \nu_a} \rho_b(E_b) \langle \psi_x^0(\vec{k}_b) | W_x | \psi_x^0(\vec{k}_b) \rangle, \quad (3)$$

where v_a is the projectile-target relative velocity, $\rho_b(E_b) = k_b \mu_b / [(2\pi)^3 \hbar^2]$ is the density of the states for the projectile b, W_x is the imaginary part of the optical potential describing x+A elastic scattering, and $\psi_x^0(\vec{k}_b)$ is the relative state between x and A, which governs the evolution of x after the collision, when particle b is emitted with momentum \vec{k}_b and the target remains in its ground state. This state satisfies the following equation when representing on x-A relative coordinates \vec{r}_x , where the relevant coordinates are depicted in Fig. 1

$$\langle \vec{r}_x | \psi_x^0(\vec{k}_b) \rangle = \int_0^\infty d\vec{r}_x' G_x(\vec{r}_x, \vec{r}_x') \langle \vec{r}_x' \chi_b(\vec{k}_b) | V_{\text{post}} | \Psi^{3b} \rangle, \quad (4)$$

where $G_x = 1/(E_x^+ - H_x)$ with the internal Hamiltonian $H_x = T_x + U_x$ of x - A subsystem and the relative energy E_x between particles x and A, χ_b is the distorted-wave describing the scattering of b in the final channel with respect to the x - A subsystem, $V_{\text{post}} = V_{bx} + U_{bA} - U_b$ (with U_b the optical potential describing the relative motion between the b and B^* in the outgoing channel) and Ψ^{3b} is the three-body wave function, with boundary conditions corresponding to the incident a particle.

Austern *et al.* [18] suggested using the CDCC wave function to approximate the three-body wave function, Ψ^{3b} , appearing in Eq. (4). Since the CDCC wave function is also a complicated object which contains different partial wave components for the b-x subsystem, one needs to treat each partial wave equally. In previous works [7,13], we have tested the validity of $\ell=0$ case (deuterons and $^6\mathrm{Li}$) by employing the distorted-wave Born approximation (DWBA), i.e., $\Psi^{3b}=\chi_a^{(+)}\phi_a$, where $\chi_a^{(+)}$ is the distorted wave describing the a+A elastic scattering and ϕ_a is the projectile ground state wave function, and compared the calculation results with experimental data. However, the IAV model has never been applied and tested for $\ell \geqslant 1$ cases. For that purpose, I will focus on $\ell=1$ case with $^7\mathrm{Li}$.

Instead of using a three dimensional Jacobi basis, one can expand the wave function into partial wave eigenstates which depend on the magnitude of the radius and angular momentum eigenstates. The orbital angular momenta of three particles are coupled to total angular momentum J and its third component, for the incoming channels

$$|r_{bx}r_a\alpha_{\rm in}\rangle = |r_{bx}r_a((l_a(j_bj_x)s_{bx})J_a(\lambda_aj_A)J_A)JM_J\rangle_{\rm in}, \quad (5)$$

and for the outgoing channels

$$|r_x r_b \alpha_{\text{out}}\rangle = |r_x r_b((l_x(j_x j_A) s_{xA}) J_x(\lambda_b j_b) J_b) J M_J\rangle_{\text{out}},$$
 (6)

where j_b , j_x , and j_A are the internal spins of particles b, x, and A, respectively, s_{bx} and s_{xA} are the total spins of subsystem in incoming and outgoing channels, respectively, l_a , λ_a , l_x , and λ_b are the relative angular momentum of b-x, a-A, x-A, and $b-B^*$, respectively, and J_a (J_A) and J_x (J_b) are the total angular momentum of subsystem (spectator) in incoming and outgoing channels, respectively.

The angular momentum basis can be normalized as

$$\langle r'_{bx}r'_{a}\alpha'_{\rm in}|r_{bx}r_{a}\alpha_{\rm in}\rangle = \frac{\delta(r'_{bx} - r_{bx})}{r'_{bx}r_{bx}} \frac{\delta(r'_{a} - r_{a})}{r'_{a}r_{a}} \delta_{\alpha'_{\rm in},\alpha_{\rm in}}, \quad (7)$$

and likewise for the outgoing basis.

In addition to that, a two-body angular momentum basis for the x-A subsystem is used,

$$|r_x \beta\rangle = |r_x(l_x s_{xA}) J_x M_x\rangle, \tag{8}$$

therefore, the three-body outgoing state can be decoupled by

$$|r_x r_b \alpha_{\text{out}}\rangle = \sum_{M_x M_b} \langle J_x M_x J_b M_b | J M_J \rangle |r_x \beta \rangle |r_b J_b M_b \rangle, \quad (9)$$

as well as the incoming state

$$|r_{bx}r_a\alpha_{\rm in}\rangle = \sum_{M_aM_A} \langle J_aM_aJ_AM_A|JM_J\rangle |r_{bx}J_aM_a\rangle |r_aJ_AM_A\rangle,$$
(10)

where M_x , M_b , M_a , and M_A are the third component of J_x , J_b , J_a , and J_A , respectively.

By using the angular momentum basis defined above, one can rewrite Eq. (4) as

$$\langle r_x \beta | \psi_x^0(\vec{k}_b) \rangle = \int_0^\infty dr_x' r_x'^2 G_x(r_x, r_x', \beta) \rho(r_x', \beta, \vec{k}_b)$$
 (11)

with

$$\rho(r_x', \beta, \vec{k}_b) = \langle r_x' \beta \chi_b^{(-)}(\vec{k}_b) | V_{\text{post}} | \chi_a^{(+)} \phi_a \rangle. \tag{12}$$

Since the incoming and outgoing channels are represented in their natural set of Jacobi coordinate (see Fig. 1). A transformation from the sets $|r_{bx}r_a\alpha_{\rm in}\rangle$ to $|r_xr_b\alpha_{\rm out}\rangle$ is required. A partial wave representation of this transformation is outlined in Ref. [19] and can be written as an integration over the cosine of the relative angle between \vec{r}_x and \vec{r}_b . All geometrical information is included in the coefficients $\mathcal{G}_{\alpha_{\rm in},\alpha_{\rm out}}^{\rm out\leftarrow in}(r_xr_bx)$. More details on these transformation are given in the Appendix. Additionally, I only consider a central potential for U_{bA} . Then inserting complete set of states in Eq. (12) and making use of the geometrical coefficients $\mathcal{G}_{\alpha_{\rm in},\alpha_{\rm out}}^{\rm out\leftarrow in}(r_xr_bx)$, one should arrive at the following result:

$$\rho(r_x', \beta, \vec{k}_b) = \sum_{\alpha_{\text{out}}} \int_0^\infty dr_b' r_b'^2 \langle r_x' \beta \chi_b^{(-)}(\vec{k}_b) | r_x' r_b' \alpha_{\text{out}} \rangle$$

$$\times \sum_{\alpha_{\text{in}}} \int_{-1}^1 dx V_{\text{post}}(r_x' r_b' x \alpha_{\text{in}}) \mathcal{G}_{\alpha_{\text{in}}, \alpha_{\text{out}}}^{\text{out} \leftarrow \text{in}}(r_x' r_b' x)$$

$$\times \langle r_{bx} r_a \alpha_{\text{in}} | \chi_a^{(+)} \phi_a \rangle$$
(13)

with

$$\langle r_x' \beta \chi_b^{(-)}(\vec{k}_b) | r_x' r_b' \alpha_{\text{out}} \rangle$$

$$= \sum_{M_x M_b} \langle J_x M_x J_b M_b | J M_J \rangle \langle \chi_b^{(-)}(\vec{k}_b) | r_b J_b M_b \rangle \delta_{\beta, J_x M_x}$$
(14)

and

$$\langle r_{bx}r_a\alpha_{\mathrm{in}}|\chi_a^{(+)}\phi_a\rangle = \sum_{M_a'M_A}\langle J_aM_a'J_AM_A|JM_J\rangle\langle r_{bx}J_aM_a'|\phi_a\rangle$$

$$\times \langle r_a J_A M_A | \chi_a^{(+)} \rangle. \tag{15}$$

It should be noted that, in the above representation, r_{bx} and r_a are functions of r'_x , r'_b , and x (details are given in the Appendix).

The double differential cross section of NEB, which given by Eq. (3) can be represented with the angular momentum basis as

$$\begin{split} \frac{d^2\sigma}{dE_b d\Omega_b} \Big|_{\text{NEB}} &= -\frac{2}{\hbar \nu_a} \rho_b(E_b) \\ &\times \sum_{\beta} \int_0^{\infty} dr_x r_x^2 \big| \psi_x^0(r_x, \beta, \vec{k}_b) \big|^2 W_x(r_x, \beta). \end{split} \tag{16}$$

I consider the case of unpolarized beam, and unaligned target. Moreover, I assume that the spin orientation of b is not measured. In this situation, the cross section is obtained as an average of the initial angular momentum projections of J_a and J_A , and a sum over the final projection of J_b . Thus

$$\frac{d^{2}\sigma}{dE_{b}d\Omega_{b}}\Big|_{\text{NEB}} = -\frac{2}{\hbar\nu_{a}}\rho_{b}(E_{b})\frac{1}{(2J_{a}+1)(2j_{A}+1)}\sum_{\beta}\sum_{M_{a}m_{A}m_{b}} \times \int_{0}^{\infty} dr_{x}r_{x}^{2}|\psi_{x}^{0}(r_{x},\beta,\vec{k}_{b})|^{2}W_{x}(r_{x},\beta), \quad (17)$$

where m_A and m_b are the third components of j_A and j_b , respectively. The main difference of the present method, compared to previous implementations of the IAV model [7,8,13], lies in the coordinate transformation. This new method is numerically more efficient for high relative angular momenta between the fragments. This, in turn, should facilitate its extensions beyond the DWBA formula, for example, using CDCC three-body wave functions for the initial state, as proposed in the original work of Austern *et al.* [18].

III. CALCULATIONS

A. 58 Ni(7 Li, αX)

To assess the validity of this partial wave expansion, I have done the benchmark calculation comparing our earlier expansion given in Ref. [7]. The numerical difference between these two method is less than 1% when using the same input parameters. On the other hand, due to the well-known convergence problems of the DWBA post-form formula [arising from the long-range behavior of $\rho(r'_x,\beta,\vec{k}_b)$ in Eq. (12)], I adopt here the equivalent prior-form representation [8,21], which is free of these problems.

Now I present calculations for reactions induced by a ⁷Li projectile and compare the calculated inclusive cross sections with experimental data to assess the validity of the theory. In this case, I compute the separate contributions for the elastic (EBU) and nonelastic (NEB) breakup cross sections. For the former, I use the CDCC formalism, using the coupled-channels code FRESCO [22]. This makes it possible to treat the EBU to all orders and should be equivalent to the post-form three-body model of Austern *et al.* For the NEB part, I use the DWBA version.

I consider the reaction ⁵⁸Ni ($^7\text{Li}, \alpha X$) at energies around Coulomb barrier, which allows us to compare with data from Ref. [17]. The ^7Li nucleus is treated in a two-cluster model ($\alpha + t$). Compared to the ($\alpha + d$) two-cluster structure of ^6Li , the main difference between the two nuclei is the internal angular momentum ℓ , for ^6Li $\ell = 0$, whereas for ^7Li $\ell = 1$. Furthermore, the difference in the breakup threshold energy of the two Li isotopes, 1.474 MeV for $\alpha + d$ breakup of ^6Li compares to 2.468 MeV for the $\alpha + t$ breakup of ^7Li is also important.

In order to test the validity of the $\alpha + t$ two cluster model for ⁷Li, first the elastic scattering of the same reaction was studied using the CDCC framework. The $\alpha + t$ interaction, which is required to generate the ⁷Li ground state wave function as well as the bound excited state and continuum wave functions, was taken from Ref. [23]. This potential consists of a central and a spin-orbit component, of Gaussian shape, with a fixed geometry and a parity-dependent depth. The potential well depths were adjusted to give the correct binding energy and resonance energy for bound and resonant states, respectively. In order to achieve convergence of the calculated cross sections, one needed to include $\alpha + t$ partial waves up to $\ell = 3$. For the f wave, a finer division of bins is used in order to reproduce the $\ell = 3$ resonant states at 4.63 MeV $(7/2^{-})$ and 6.68 MeV $(5/2^{-})$ correctly. The ⁴He-target interaction was obtained from a Woods-Saxon potential fitted to the 12 MeV 4 He + 58 Ni elastic

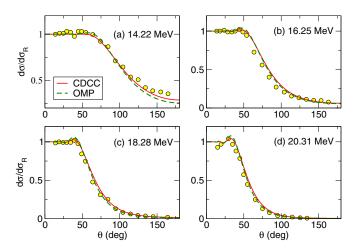


FIG. 2. Elastic scattering of ⁷Li + ⁵⁸Ni at different incident energies. The solid and dashed lines are the CDCC calculations and the optical model calculation with the OMP of Cook [20], respectively. Experimental data are taken from Ref. [17].

scattering data of Ref. [24] with the following parameters: V=49.5 MeV, $R_0=5.88$ fm, $a_0=0.5$ fm, W=11.0 MeV, $R_w=5.69$ fm, and $a_w=0.5$ fm. The 3 He-target interaction was taken from the 8.95 MeV $t+^{58}$ Ni parameters of Ref. [25]. For comparison, the optical model calculation using the potential of Cook[20] was also performed. Figure 2 shows the elastic scattering of 7 Li + 58 Ni at different incident energies. The data are taken from Ref. [17]. The solid and dashed lines are, respectively, the CDCC and optical model calculations. It can be seen that both the optical model and CDCC calculations reproduce well the experimental data. This agreement confirms the validity of the adopted α + target and t + target optical potentials.

Now the inclusive breakup cross section (${}^{7}\text{Li}, \alpha X$) is discussed. The EBU part was obtained from the CDCC calculation discussed above. The NEB part was calculated with the IAV model using the DWBA formalism without taking account the spin of particles. There are two distinct contributions to the NEB cross sections, namely, that for $E_x > 0$ case and that for $E_x < 0$ case, where E_x is the final relative energy between t and 58 Ni. For $E_x < 0$, this region would correspond to bound states of the residual ⁶¹Cu system, that is, transfer. The application of NEB formalism to transfer reactions is outlined in Ref. [26] and has been recently applied to deuterons and ⁶Li induced reactions [10,13]. In Fig. 3 the dotted, dashed, and dot-dashed lines are, respectively, the EBU (CDCC), NEB (DWBA) with $E_x < 0$, and NEB (DWBA) without $E_x < 0$ components. First, it is noticeable that the EBU part is negligible compared to the NEB component, which is in contrast to ⁶Li as reported in Ref. [13]. For the ⁶Li case, the contribution of EBU is small but non-negligible comparing to NEB. The difference of these two nuclei will be discussed in the following section. Concerning the comparison of the calculations with experimental data, one can observe a good agreement with the data when including the E_x < 0 part for higher two energies and excluding the $E_x < 0$ for lower two energies. The reason of that is not completely clear but it might be due to the

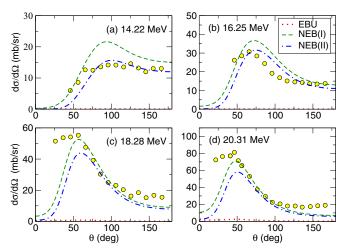


FIG. 3. Angular distribution of α particles produced in the reaction $^7\text{Li} + ^{58}\text{Ni}$ at the incident energies indicated by the labels. The dotted, dashed and dot-dashed are, respectively, the EBU, NEB with $E_x < 0$, and NEB without $E_x < 0$ components. The experimental data are taken from Ref. [17].

fact that an energy-independent $t+^{58}{\rm Ni}$ potential has been employed, which will not describe correctly the low energy region (including the bound state part) of this system. A more realistic description should be provided by a energy-dependent potential, extending also to negative energies. Such potentials were investigated in the past by Mahaux and Sartor [27] and are currently being revisited by several groups (see Ref. [28] for a recent review).

B. Comparison with the ⁶Li case

In this section, the difference between ⁶Li and ⁷Li on the ⁵⁸Ni target is discussed. The calculations of ⁶Li have been presented in Ref. [13]. In both cases, one should find that the NEB¹ component dominate the inclusive α s. However it is interesting to compare the relative importance of EBU versus NEB on these two nuclei. In order to make a more meaningful comparison with these two nuclei, a toy model of ⁶Li is introduced by modifying the binding energy from $E_b = -1.474$ MeV to $E_b = -2.468$ MeV (that is, the ⁷Li binding energy). Figure 4 (a) plots the ration of the calculated EBU and TBU (=EBU+NEB) cross section as a function of the reduced energy $E_{\rm c.m.}/V_B$, with V_B the energy of the Coulomb barrier, estimated as $V_B = Z_p Z_t / [r_B (A_t^{1/3} + A_p^{1/3})]$, where $Z_p(Z_t)$ and $A_p(A_t)$ are the atomic number and atomic mass of projectile (target), respectively, and $r_B = 1.44$ fm. The circles, squares and diamonds are, respectively, ⁶Li + ⁵⁸Ni, 6 Li^{toy} + 58 Ni, and 7 Li + 58 Ni reaction systems. Several interesting features emerge from this plot: (i) First, for the lower binding energy, i.e., ${}^6{\rm Li} + {}^{58}{\rm Ni}$, the elastic breakup component becomes more important as the energy decreases, whereas for the energies above the Coulomb barrier, the ratio shows an

¹Note that these NEB includes both $E_x > 0$ and $E_x < 0$ contributions.

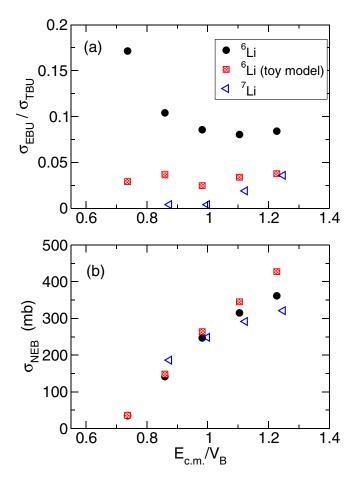


FIG. 4. (a) Ratios of EBU over TBU (=EBU+NEB) for $^{6.7}$ Li + 58 Ni systems. (b) NEB cross sections for $^{6.7}$ Li + 58 Ni systems. See text for details.

almost constant behavior; (ii) second, when increasing the binding of projectile, i.e., ⁶Li^{toy} + ⁵⁸Ni, the elastic breakup component becomes comparatively smaller; (iii) third, when changing the relative angular momentum in the projectile from $\ell = 0$ to $\ell = 1$, i.e., ⁷Li + ⁵⁸Ni, the importance of elastic breakup component is the smallest in these three systems and increases with the incident energy. These results can be attributed to the fact that the EBU is a peripheral process and thereby highly sensitive to the tail of projectile wave function. In Fig. 5, it can be clearly seen that ⁶Li has the longest tail among these three systems and this explains the larger EBU contribution. By contrast, due to the larger binding energy and centrifugal barrier, the wave function of ⁷Li is comparatively more confined at small distances. This short tail behavior makes the ⁷Li projectile difficult to break at these low energies.

Figure 4(b) shows the NEB cross sections as a function of the reduced energy $E_{\rm c.m.}/V_B$. It can be seen that the NEB cross section for these three systems are of similar magnitude. This indicates the NEB depends on the internal region of the projectile wave function where these three projectile have the similar structure as pointed out in Fig. 5. This agrees with the results of Ref. [12], where we have compared the

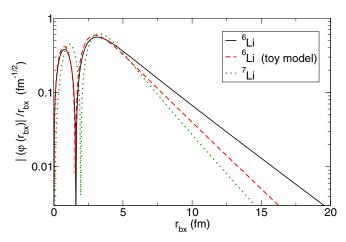


FIG. 5. Projectile wave functions for ^{6,7}Li. See text for details.

relative importance of EBU and NEB with ⁶Li projectile when artificially changing the binding energy.

IV. SUMMARY AND CONCLUSIONS

In summary, I have addressed the calculation of inclusive breakup cross sections for arbitrary ℓ values (with ℓ the orbital angular momentum between the clusters in the projectile ground state) within the closed-form DWBA model proposed in the 1980s by Ichimura, Austern, and Vincent [6]. A novel numerical implementation of the model, more suitable for $\ell > 0$ values, has been presented here.

I have performed calculations for the 58 Ni(7 Li, αX) reaction at energies around the Coulomb barrier. In this case, one can find a good agreement between the experimental data and the IAV model.

I have also investigated the effect of the internal structure of the projectile by comparing the $^7\mathrm{Li}$ inclusive breakup with $^6\mathrm{Li}$. Although in both cases the α inclusive cross section is dominated by the NEB component, the EBU part is comparatively larger for the $^6\mathrm{Li}$ case. one can interpret this as a consequence of the larger extension of the $^6\mathrm{Li}$ ground state wave function, due to its $\ell=0$ configuration.

The results presented in this work, along with those presented in previous works [7,8,13], indicate that the IAV model provides a reliable framework to calculate NEB cross sections. Possible applications to knockout reactions at intermediate energies are currently under study.

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APPENDIX: GEOMETRICAL COEFFICIENT FOR COORDINATE TRANSFORMATION

In this section, I present the explicit expressions of the geometrical coefficients $\mathcal{G}_{\alpha_{in},\alpha_{out}}^{\text{out}\leftarrow \text{in}}(r'_xr'_bx)$. These are given by

$$\mathcal{G}_{\alpha_{\text{in}},\alpha_{\text{out}}}^{\text{out}\leftarrow\text{in}}(r_x'r_b'x) = \sum_{LS} (2S+1)\sqrt{(2J_a+1)(2J_A+1)(2J_x+1)(2J_b+1)} \begin{cases} l_x & s_{xA} & J_x \\ \lambda_b & j_b & J_b \\ L & S & J \end{cases} \begin{cases} l_a & s_{bx} & J_a \\ \lambda_a & j_A & J_A \\ L & S & J \end{cases}$$

$$\times 8\pi^2 \sum_{M=-L}^{L} \left\{ Y_{l_x}^{m_{l_x}*}(\hat{r}_x) Y_{\lambda_b}^{m_{\lambda_b}*}(\hat{r}_b) \right\}^{LM} \left\{ Y_{l_a}^{m_{l_a}}(\widehat{ar_x - r_b}) Y_{\lambda_a}^{m_{\lambda_a}}(\widehat{br_x + cr_b}) \right\}^{LM}$$

$$\times (-)^{s_{bx}+2j_A+j_x+j_b} \sqrt{(2s_{xA}+1)(2s_{bx}+1)} \begin{cases} j_A & j_x & s_{xA} \\ j_b & S & s_{bx} \end{cases} . \tag{A1}$$

The spherical harmonics $Y_l^m(\hat{r})$ depend on the angles \hat{r} of the vector \vec{r} . For the evaluation, one can choose \vec{r}_b as z direction and \vec{r}_x is in the x-y plane:

$$\vec{r}_b = \begin{pmatrix} 0 \\ 0 \\ r_b \end{pmatrix} \qquad \vec{r}_x = \begin{pmatrix} r_x \sqrt{1 - x^2} \\ 0 \\ r_x x \end{pmatrix} , \tag{A2}$$

where x is the cosine of the angle between \vec{r}_b and \vec{r}_x . In Eq. (A1) the curly brackets grouping the spherical harmonics indicate that they are coupled to a state of total orbital angular momentum L and third component M. The mass ratios are given by

$$a = \frac{m_A}{m_A + m_x},$$

$$b = \frac{(m_b + m_x + m_A)m_x}{(m_A + m_x)(m_b + m_x)},$$

$$c = \frac{m_b}{m_b + m_x}.$$
(A3)

For this case, the coordinates of the incoming channel are given by

$$r_{bx}(r_x r_b x) = \sqrt{a^2 r_x^2 + r_b^2 - 2ar_x r_b x},$$

$$r_a(r_x r_b x) = \sqrt{b^2 r_x^2 + c^2 r_b^2 + 2bc r_x r_b x}.$$
(A4)

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